LES4ECE CONFERENCE

June 18th, 2021

Virtual Meeting

Using machine learning to overcome the computational bottleneck of coupling injector and spray simulations



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Funding:

- U.S. Department of Energy, Michael Weismiller, Gurpreet Singh and Kevin Stork
- Laboratory Directed Research and Development (LDRD) funding from Argonne

Technical Support:

- **Convergent Science, Inc.** for providing software licenses and technical support
- LCRC and ALCF computing resources at Argonne National Laboratory
- Petro Junior Milan (Georgia Institute of Technology)
- Romit Maulik (Argonne National Laboratory)



Industry has voiced their need for accurate simulation tools that can link fuel injector and engine performance with efficiency and emissions



To address the expense of injector simulations, a data-driven emulator is used to predict the spatiotemporal injection profile



- Machine Learning models emulate internal flow fields at orifice exit
- Emulated flowfields coupled with:
 - Lagrangian spray model¹
 - Eulerian-Lagrangian Spray Atomization (ELSA) model



CFD Simulation

ML Emulator



A-M1 injector Side-oriented single-hole injector geometry

Emulated flowfields at orifice exit for static needle lift LES simulations at steady state:

- Gaseous volume fraction (*α*)
- Velocity components (*u*, *v*, *w*)
- Turbulent kinetic energy (k)
- Liquid mass (m_l)

Our recent work has focused on developing and coupling the spatiotemporal emulator with different spray models

Development of Emulator Framework





Coupling of Emulator with Lagrangian Spray Model

Time ASOI: 0.400 ms Droplet Radius [µm] 25 50 84 Temperature [K] 800 1200 1600 2000

Coupling of Emulator with ELSA Model





The construction of an emulator is organized into three phases:





Simplified injector simulations are performed that capture the salient physics of internal flow development



Model Set-up ^[2,3]			
Software	CONVERGE		
Eqs. & Turbulence	Navier-Stokes LES, Dynamic Structure Model		
Two-phase flow	Multiphase single mixture model w/ Homogeneous Relaxation Model (HRM) ^[4] Gas: compressible, RK EOS Liquid: compressible, barotropic fluid		
Mesh spacing	160 μm base grid size 5 μm min grid size in embedded regions Peak cell count: 5.4M to 6.6M cells		
Run time	1400 – 2000 CPU-hours per $10\mu s$ of simulated time. Max CFL = 0.25, dt< 1e-09 s		

[1] Milan et al., AIAA SciTech, 2021

[2] Milan et al., Atomization and Sprays, Vol. 30, 2020

[3] Torelli, Magnotti et al., SAE International, 2019

[4] Bilicki & Kestin, Proc. Royal Society London A, Vol. 428, 1990



A design of experiments approach is used to efficiently explore the set of parameters that are known to affect cavitation

Design Parameters	Range		
Static needle lift, δ [µm]	15	400	[1]
Fuel viscosity, μ_F [(N s) /m ²]	2.88×10 ⁻⁴	1.51×10^{-3}	[2]
Level of dissolved gas Y_{N_2} [-]	1×10 ⁻⁷	1×10 ⁻³	[3]

- Design of Experiments (DoE)
 - □ Variant of Latin Hypercube Sampling
 - □ 60 samples in total in 3-D design parameter space
- The blue dots (55) represent operating conditions seen during training, and the red dots (5) correspond to new operating conditions (test cases)

The test cases are chosen using input sensitivity analysis to encompass the different gas phase flow structures of the gas phase in the design space⁴

Guo et al., SAE International, 2020. [2] Magnotti and Som, ASME ICEF, 2019.
Battistoni et al., Atomization and Sprays, Vol.25, 2015. [4] Mondal et al., SAE International, 2021.



Reproduced with permission from Mondal et al., SAE Int. J. Adv. & Curr. Prac. in Mobility 3(3):1408-1424, 2021.





The autoencoder allows for faithful reconstruction of flowfields



The construction of an emulator is organized into three phases:





The emulator is comprised of deep learning-based models to relate design parameters to the predicted spatiotemporal flowfield



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The regression model is another deep neural network that maps the design variables and time to the reduced dimensional latent space





The emulator accurately captures the time-averaged flowfield



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Development of Emulator Framework





Coupling of Emulator with Lagrangian Spray Model

Time ASOI: 0.400 ms Droplet Radius [µm] 25 50 84 Temperature [K] 800 12001600 2000

Coupling of Emulator with ELSA Model



The emulator is tested by comparing the spray development using the CFD- and emulator-predicted injection profiles

Liquid Fuel	Fuel Temperature [K]	Fuel Pressure [bar]	Chamber Temperature [K]	e Chamber Density [kg/m ³]
n-dodecane*	323	1500	900	22.8
Model Set-up				
Software	CONVERGE	v2.4		
Parcel Initialization	on Static couplir	ng, LVF threshold = 0.1		
Spray breakup	KH-RT, NTC	collision model		
Turbulence	RANS, RNG	К-Е		
Combustion	<mark>UFPV</mark> – 4D t LLNL mecha	abulation (χ , c , $\widetilde{Z^{"2}}$, \widetilde{Z}) nism (2,755 species + 1	1,173 reactions)	
Mesh spacing	2 mm base g 250 µm min g Peak cell cou	jrid size grid size (AMR + Embed unt: 300,000 cells	lding)	ith permission from Mondol of
Run time	~ <mark>20 core-hou</mark> Max convect	<mark>urs</mark> per 10 μs simulated t ive-based CFL = 1.0, dt	ime al., SAE Int. J. ~ 1e-07 s 3(3):1408-1424,	Adv. & Curr. Prac. in Mobility 2021. Argonne

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The emulator provides accurate spray combustion predictions at a fraction of the cost of simulating the next design point of interest



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The emulator has also been extended to provide the injection profile for the Eulerian Lagrangian Spray Atomization model

Liquid Fuel Fuel Temperature [K]		e Fuel Pressure [bar]	Chamber Temperature [K]	Chamber Density [kg/m ³]	
n-dodecane*	323	1500	323	22.8	
Model Set-up					
Software		CONVERGE v3.0			
Eulerian Initializa	ation	Static coupling, LVF threshold	I = 0.1		
Turbulence		RANS, RNG κ-ε		and an and the state of the sta	
Spray structure		$\frac{\partial \Sigma}{\partial t} + \frac{\partial u_i \Sigma}{\partial x_i} = \frac{\partial}{\partial x_i} \left($	$\left(D_{\Sigma}\left(\frac{\partial\Sigma}{\partial x_{i}}\right)\right) + C_{\Sigma}\Sigma\left(1 - \frac{\Sigma}{\Sigma_{eq}}\right)$	$\left(-\frac{1}{2} \right) + S_{init} + S_{evap}$	
Mesh spacing Run time		160 μm base grid size40 μm min grid size (Fixed en Peak cell count: 1.48 million c	nbedding) Compar cells run tim	Compare to internal flow simulati run time: 1400 – 2000 core-hour	
		~120 core-hours per 10 µs sir Max convective-based CFL =	nulated time 1.0, dt ~ 3e-09 s	09 s)	



The emulator has been demonstrated to provide accurate spray predictions within the ELSA framework at a fraction of the cost



Error of predicted external flowfields

Field	α	v	w	V _{mag}	Σ
Error	1.5%	8.1%	3.5%	4.0%	6.5%



ONGOING RESEARCH AND FUTURE OUTLOOK



Extension of the emulator framework is underway to predict the injection profile for transient injector operation

Limitations of the current framework:

- Transient needle motion is not accounted for
- Flowfield predictions are point estimates, without any information on how much they can be trusted

Principled way of adding DoE points to Transient needle simulations reduce prediction uncertainty Training Validation Test 25 log₁₀(Y_{N2}) [-] 20 15 10 5 Latent 0.5 1.0 1.5 Space (z) $\times 10^{-3}$ μ_F [N-s/m²] Uncertainty quantification in flowfield predictions $t = 50.0 \ \mu s$ 1.0 Transfer learning 0.1 0.8 50 0.08 50 pre-trained autoencoder y[µm] 0.6 0.06 from static needle simulations $\sigma(z)$ 0.4 0.04 -50 0.2-50-0.02 Probabilistic predictions 0.0 0.0 50 50 of latent space (z) -50Ó -50 Ó Test design $x[\mu m]$ $x[\mu m]$ Design space point **Gaussian Process Standard deviation** Mean predicted a $(\delta, \mu_{F_1}Y_{N_2})$ Model in α prediction Argonne 🖌

Extension of the emulator framework is underway to predict the injection profile for transient injector operation



Emulation error of flowfields

Flowfield	α	и	v	tke	m_l	Demonstrations
Error	10%± 3%	2%± 0.5%	34%±7%	11%± 2%	3%± 1%	Showin for Case 9



The emulator provides accurate spray combustion predictions at a fraction of the cost of simulating the next design point of interest



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THANK YOU

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